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# Neutron spectrum determination at the ITER material irradiation stations at JET

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## Abstract

This paper reports new activities conducted as part of the JET technology programme under the WP-JET3 ACT sub-project collaboration. The aim of the sub-project is to take advantage of the significant 14 MeV neutron fluence expected during JET operations to irradiate samples of materials that will be used in the manufacturing of main ITER tokamak components. Here, experimental measurements of dosimetry foil activity following irradiation in JET irradiation stations have been used as input to a neutron spectrometry unfolding methodology, which is based on an iterative non-linear least squares algorithm, to derive a new neutron spectrum. The new spectra are compared to those originally derived from simulations with the JET fission yield measurements as an input. We conclude that dosimetry foil activation measurements may be used as a fluence measurement system which can complement integrated data from fission counter diagnostics, but with an additional benefit that useful spectrum information may be extracted, particularly above 2 MeV.

*Keywords:* activation, neutronics, fusion

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## 1. Introduction

The experiments that are planned over the next few years at the Joint European Torus (JET), notably including a deuterium-tritium (D-T) experimental phase, are expected to produce large neutron yields,

up to  $1.7 \times 10^{21}$  neutrons. The scientific objectives of the experiments are linked with a technology programme, WPJET3, to deliver the maximum scientific and technological return from those operations, with particular emphasis on technology exploitation via the high neutron fluxes predicted in and around the JET machine. The experimental data expected to be retrieved will help to develop and improve the radiation transport and activation simulation capabilities via benchmarking and validation studies in

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fusion tokamak relevant operational conditions. Significant results have been obtained to date with a focus on relevance to ITER device operations [1]. Nuclear activities that have been performed include the 14 MeV calibration of neutron yield monitors [2], neutronics benchmark experiments [3, 4, 5, 6, 7], nuclear diagnostics and data processing for tritium breeding blankets [8], and activation measurements with supporting analyses for fusion materials [9, 10, 11] for example.

This paper describes some of the latest activities performed under the neutron activation sub-project known as ACT, which has the aim to irradiate a range of real ITER materials in JET experiments and obtain valuable nuclear response benchmark data from those materials. Whilst the main theme of this paper focusses on neutron spectrometry methodology and its application to a large set of dosimetry foil activity measurements obtained in a previous JET campaign, progress towards the next major phase of the sub-project has been made, which is expected to see ITER material samples irradiated in the forthcoming JET deuterium-deuterium (D–D) campaign expected in late 2018. A selection of ITER materials samples for use in the sub-project have been collected by Fusion for Energy. These include: poloidal field (PF) coil jacket and toroidal field coil radial closure plate steels, EUROFER 97-3 steel, W and CuCrZr materials from the divertor, Inconel 718, CuCrZr and 316L stainless steel for blanket modules, vacuum vessel forging samples and NbSn toroidal field coil strands, for example. A number of disc sub-samples have now been cut from the bulk material and installed into JET for the D–D campaign. The newly prepared long-term irradiation station (LTIS) assembly, with 26 positions containing the samples, are shown in figure 1 alongside one of the LTIS assemblies used in the experiments discussed in this paper.

Full details of the collaborative work performed in previous experiments, which supported characterisation of the LTISs that were used in a 2015–16 JET D–D campaign are detailed in [11]. In summary, 176 high-purity dosimetry foils were irradiated in the LTIS in JET octants 4 and 8. These foils were then distributed to four EU laboratories for measurement using high resolution gamma spectrometry sys-



Figure 1: (LHS image) LTIS assembly using on 2015-16 campaign prior to installation and irradiation; (RHS image) New LTIS assembly sample holder containing ITER materials and dosimetry foils prior to installation into JET in 2018.

tems. Activity predictions obtained using neutron transport and activation simulations using an updated JET radiation transport model were compared against experimental activity measurements. Conclusions from the previous work [11] showed that the models and simulation approach that was taken is broadly satisfactory for most of the threshold reactions that were studied with an average C/E (calculated over experimental ratio result) of  $0.91 \pm 0.01$  (see figure 2). However, two groups of reactions yielded low C/E, suggesting that parts of the calculated LTIS neutron spectrum can be improved, given that all of these reaction cross sections are considered to be well known and therefore included in the international reactor dosimetry file for fusion and fission (IRDF). A set of four capture reactions,  $^{58}\text{Fe}(n,\gamma)^{59}\text{Fe}$  reaction,  $^{45}\text{Sc}(n,\gamma)^{46}\text{Sc}$  reaction,  $^{59}\text{Co}(n,\gamma)^{60}\text{Co}$  and  $^{181}\text{Ta}(n,\gamma)^{182}\text{Ta}$  reactions all exhibited low C/E values (with a weighted average C/E value across the four sets of measurements of 0.66) suggesting that the thermal neutron flux is under-predicted in the calculated results. It should be noted that an alternative MCNP model, developed for other aspects of JET nuclear analysis with some differences in Be mass and geometry (for a poloidal limiter component) in the vicinity of the LTIS for example, predicts significantly higher neutron fluences, by approximately a factor of 2, at thermal energies in the LTIS region. The model selected for the calculation results presented in this work (also discussed in more detail

in [11]) is thought to contain a more accurate representation of the Be limiter and total mass. However, we recognise that there may be additional material features that influence the thermal part of the spectrum that we ideally need to capture in an improved model. The deviations between the two models at low energy highlight the relatively large degree of uncertainty in modelling this particular energy region, whereas at energies above 1 MeV the agreement in fluence is within 12%. The  $^{89}\text{Y}(n,2n)^{88}\text{Y}$  reaction—a high energy threshold sensitive to neutron energies produced in D–T reactions, but not to neutron energies produced via D–D reactions—exhibited a low weighted average C/E value of  $0.67 \pm 0.2$  (see figure 2). This particular reaction is therefore a useful diagnostic of the D–T contribution within the neutron spectrum. One explanation for the low C/E values is that the D–T 14 MeV contribution for the D–D experimental campaign may typically be in the range 0.5–1.5%. In our previous calculations an indicative value of 1% was used, though based on our findings we recognise that this value should be revised for this particular experimental campaign. The motivation for this paper follows from these observations and the intention here is to use the experimental results previously obtained, together with an unfolding code and relevant response functions, to revise some energy regions of the calculated LTIS spectrum using an unfolding code in order to obtain improved C/E results across all of the 11 reactions that were measured.

## 2. Neutron spectrometry methodology

In this work standard inverse problem neutron spectrometry techniques have been performed using methodologies that have been covered extensively in previous literature, for example see [12, 13, 14, 15]. The governing equation is:

$$M_{0n} = \sum_{k=1}^{G_{tot}} R_{n,k} \phi_k,$$

where for an activation foil-based measurement  $M_{0n}$  is the measured reaction rate for the  $n$ th reaction

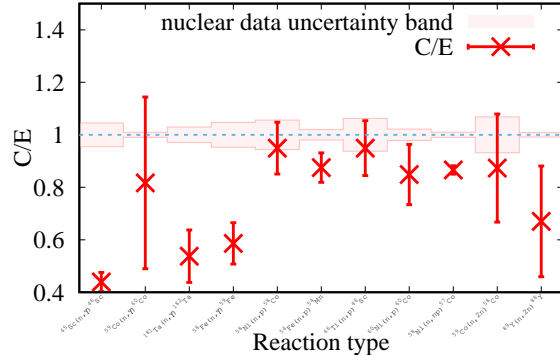


Figure 2: C/E plot for all 11 reactions measured during the experimental campaign. The error bars are the combined measurement uncertainty for each reaction type. The uncertainty band shown is the nuclear data uncertainty for each reaction.

type,  $R_{n,k}$  is the response function for the  $n$ th reaction type as a function of neutron energy, in  $G_{tot}$  energy bins, and  $\phi_k$  is the neutron flux energy spectrum, also in  $G_{tot}$  energy bins.

Here, a flexible, modern beta code based on the class of algorithms used in SAND-II [14] and the modified variant GRAVEL [12, 13] has been developed and applied to the data. Two suites of unfolding codes have been developed by UKAEA which are being tested, this work forming part of those tests. A serial code has been written in Python has been used to test the unfolding algorithm and visualise the unfolding process. The other, written in C++, includes a much faster parallelised version which implements a Monte Carlo method for uncertainty propagation and estimation of the condition of the inverse problem given the matrices provided. The main solver used by both of these codes is a non-linear least-squares minimisation method which use an iterative gradient approach to provide an improved solution. An *a priori* spectrum is used as an initial solution which is evolved to a new spectrum with each iteration. For a set of  $N$  reaction rate measurements  $\chi^2$  is calculated at each spectrum iteration,

$$\chi^2 = \sum_{n=1}^N \left( \frac{M_{0n} - M_n}{\epsilon_{M_{0n}}} \right)^2,$$

where  $M_n$  is the theoretical reaction rate and  $\epsilon_{M_{0n}}^2$  is the uncertainty in measured reaction rate,  $M_{0n}$ .

$\chi^2$  is progressively reduced by a maximum gradient method, until a solution convergence criteria set by the user is reached. Three termination criteria are available, which may be flexibly set: (i) the  $\chi^2$  per degree of freedom is reduced to a user-set target value (normally this is set to 1 or below), (ii) the largest change in flux in an energy bin within the range of interest across an iteration falls below a user-set value, or (iii) a pre-defined number of iterations have been completed.

### 2.1. Measured reaction rate data and fluence rate corrections

The 176 foil measurements performed by the four laboratories span 11 reaction types. For the  $n$ th reaction type an average activity value has been derived,  $A_n$ , and corresponding uncertainty,  $\epsilon_{A_n}$ , at a reference point in time (the end of the JET experimental campaign) by combining individual activity measurements inversely weighted by the square of the corresponding experimental uncertainty. Each  $A_n$  is then used to determine a corresponding  $M_{0n}$  using

$$M_{0n} = \frac{A_n}{(1 - \exp^{-\lambda_n T})k_n}.$$

Because the actual fluence rate during irradiation varied from shot to shot a neutron fluence rate correction factor,  $k_n$ , for the  $n$ th reaction type has been calculated using FISPACT-II [16] at the end of the full irradiation period and applied to calculate  $M_{0n}$ .  $M_{0n}$  can be viewed as a time-averaged reaction rate. The irradiation-decay scheme during the JET experimental campaign was complex: a total yield of  $2.26 \times 10^{19}$  neutrons were generated in 3682 experimental JET shots over a period of 446 days. In general, for a series of  $m$  distinct irradiation shots, each  $k_n$  value may be calculated using,

$$k_n = \frac{\sum_{i=1}^m \phi_i (1 - e^{-\lambda_n \Delta t_i}) e^{-\lambda_n T_i}}{\phi (1 - e^{-\lambda_n T})},$$

where  $\Delta t_i$  is the time duration of the  $i$ th irradiation,  $T_i$  is the time from the end of the  $i$ th irradiation to the end of the total irradiation period,  $\phi_i$  is the

average neutron fluence rate for the  $i$ th irradiation period,  $\lambda_n$  is the half life associated with the reaction product nuclide from the  $n$ th reaction type and  $\phi$  is the averaged fluence rate across the total irradiation time,  $T$ .

For the JET LTIS experimental data set the above quantities have been derived from the measurements. Table 1 shows, for each reaction type,  $A_n$ ,  $k_n$ ,  $M_{0n}$  and  $\epsilon_{M_{0n}}$ .

### 2.2. Dosimetry foil response functions

Figure 3 shows a plot of the 11 response functions,  $R_{n,k}$ , associated with the dosimetry foils used in the experiments. These have been calculated in units of  $\text{cm}^2 \text{g}^{-1}$  using IRDFFv1.05 cross section data libraries, with the exception of the  $^{58}\text{Ni}(n,n'p)^{57}\text{Co}$  reaction, which does not currently exist in the IRDFFv1.05 library, and in this case nuclear cross section data from the TENDL-2015 nuclear data library has been used instead. Response functions are calculated from the microscopic cross section for the  $n$ th reaction,  $\sigma_{n,k}$ , processed into  $k = 709$  neutron energy groups,

$$R_{n,k} = \frac{N_A \sigma_{n,k} F}{A},$$

where  $N_A$  is Avogadro's constant,  $F$  is the target isotope fractional elemental abundance and  $A$  is the atomic weight of the elemental dosimetry foil target.

### 2.3. A priori neutron spectrum

The *a priori* neutron spectrum is as defined in [11] and is used as input to the unfolding code. It was calculated with the Monte Carlo-based radiation transport code MCNP-6.1 [17] with an updated JET MCNP model containing a geometric representation of the long-term irradiation assembly (also see a description of the MCNP model in more detail in [11]). The purpose of the MCNP simulations were to determine via calculation a representative neutron spectrum within the assembly. The *a priori* spectrum is shown, together with a final unfolded spectrum (explained in the next section), in figure 4.

Table 1: Table showing reaction type,  $A_n$ ,  $k_n$ ,  $M_{0n}$  and  $\epsilon_{M_{0n}}$ .

| Foil | Reaction type                                                                    | $A_n$ (Bq) | $k_n$ | $M_{0n}$ ( $s^{-1} g^{-1}$ ) | $\epsilon_{M_{0n}}$ ( $s^{-1} g^{-1}$ ) |
|------|----------------------------------------------------------------------------------|------------|-------|------------------------------|-----------------------------------------|
| Sc   | $^{45}\text{Sc}(n,\gamma)^{46}\text{Sc}$                                         | 1.397E+04  | 1.87  | 7.659E+03                    | 6.394E+02                               |
| Co   | $^{59}\text{Co}(n,2n)^{58}\text{Co}$                                             | 1.182E+02  | 2.04  | 5.876E+01                    | 1.386E+01                               |
|      | $^{59}\text{Co}(n,\gamma)^{60}\text{Co}$                                         | 3.585E+03  | 1.03  | 2.349E+04                    | 9.412E+03                               |
| Ta   | $^{181}\text{Ta}(n,\gamma)^{182}\text{Ta}$                                       | 3.062E+04  | 1.60  | 2.058E+04                    | 3.835E+03                               |
| Fe   | $^{58}\text{Fe}(n,\gamma)^{59}\text{Fe}$                                         | 6.737E+00  | 2.70  | 2.500E+00                    | 3.360E-01                               |
|      | $^{nat}\text{Fe}(n,x)^{54}\text{Mn}$ ; ( $^{54}\text{Fe}(n,p)^{54}\text{Mn}$ )   | 2.931E+01  | 1.19  | 3.922E+01                    | 2.523E+00                               |
| Ti   | $^{nat}\text{Ti}(n,x)^{46}\text{Sc}$ ; ( $^{46}\text{Ti}(n,p)^{46}\text{Sc}$ )   | 4.407E+00  | 1.83  | 2.470E+00                    | 2.724E-01                               |
| Ni   | $^{nat}\text{Ni}(n,x)^{58}\text{Co}$ ; ( $^{58}\text{Ni}(n,p)^{58}\text{Co}$ )   | 1.374E+03  | 2.04  | 6.820E+02                    | 7.100E+01                               |
|      | $^{nat}\text{Ni}(n,x)^{60}\text{Co}$ ; ( $^{60}\text{Ni}(n,p)^{60}\text{Co}$ )   | 5.460E-01  | 1.03  | 3.577E+00                    | 4.845E-01                               |
|      | $^{nat}\text{Ni}(n,x)^{57}\text{Co}$ ; ( $^{58}\text{Ni}(n,n'p)^{57}\text{Co}$ ) | 2.878E+01  | 1.22  | 3.470E+01                    | 6.387E-01                               |
| Y    | $^{89}\text{Y}(n,2n)^{88}\text{Y}$                                               | 1.012E+02  | 1.63  | 6.566E+01                    | 2.069E+01                               |

### 3. Neutron spectrum unfolding results

Figure 4 shows the *a priori* spectra and final unfolded spectra following iteration through the unfolding process. Here, the calculation was preformed for 5000 iterations, resulting in a reduction in  $\chi^2$  for the final spectrum by a factor of 25 compared to the *a priori* spectrum.

The total neutron fluence at the LTIS position for the full 446 day irradiation period was calculated to be  $1.06 \times 10^{14}$  n  $\text{cm}^{-2}$  using the *a priori* spectrum together with the KN1 JET fission chamber diagnostic system neutron yield measurement as an input. The KN1 system consists of three pairs of  $^{235}\text{U}$  and  $^{238}\text{U}$  fission chambers mounted on vertical magnetic limbs in octants 2, 6, and 8 at JET, and serves to measure the absolute neutron yield from the JET plasma and its variation in time.

Following the unfolding procedure described above the final calculated spectrum fluence was calculated to be  $1.66 \times 10^{14}$  n  $\text{cm}^{-2}$ , a factor of 1.57 higher. It is helpful to sub-divide this fluence ratio factor into three distinct energy ranges: 0–2 MeV, 2–10 MeV and above 10 MeV, to broadly understand which parts of the energy spectrum exhibit the largest differences. The ratios are calculated to be 1.82, 1.08 and 1.1 for these energy ranges respectively, showing that the greatest fluence difference between the calculated *a priori* spectrum and the unfolded spectrum is in the region below 2 MeV, whereas in the higher energy regions above 2 MeV better agreement is obtained, between 8–10%.

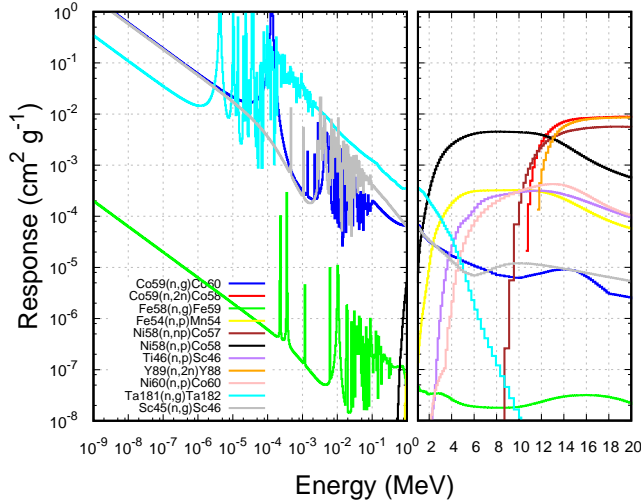


Figure 3: Plot of the 11 calculated response functions associated with the dosimetry foil reactions measured in the experiments. Note the split, logarithmic–linear, x-scale.

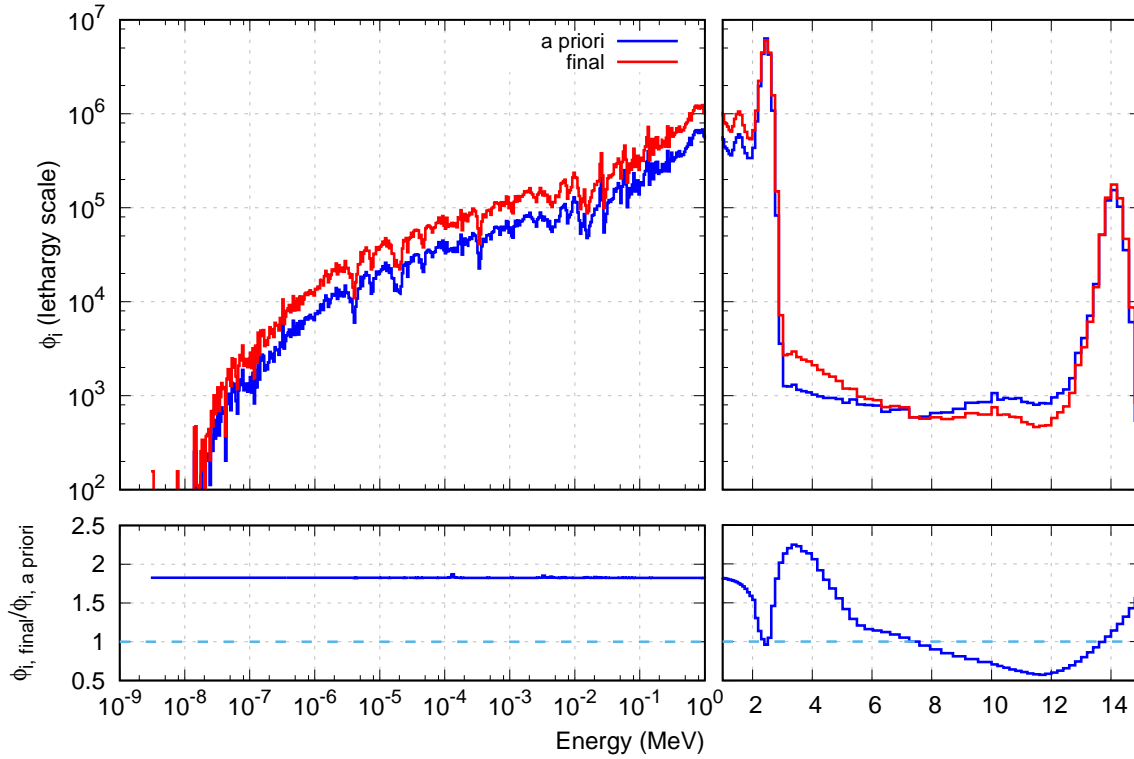


Figure 4: (top section) A-priori neutron spectrum and final spectrum after unfolding. (bottom section) differential ratio plot the two spectra. Note the split, logarithmic-linear, x-scale.

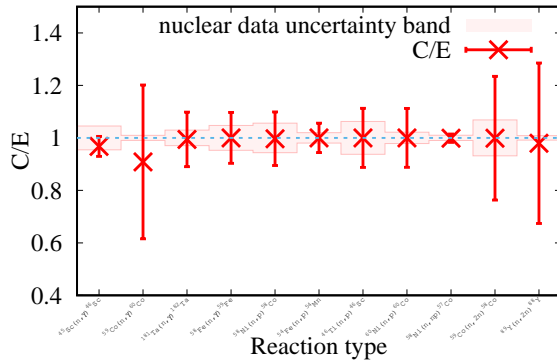


Figure 5: C/E plot for all 11 reactions measured during the experimental campaign using the final spectrum. The error bars are the combined measurement uncertainty for each reaction type. The uncertainty band shown is the nuclear data uncertainty for each reaction.

The equivalent set of C/E data across all reactions to those shown in figure 2 but with using the final, unfolded spectrum as input is shown in figure 5. One can observe that the level of agreement has significantly improved in comparison to the results shown earlier in figure 2.

#### 4. Discussion and conclusions

Activity measurements of 176 neutron activated dosimetry foils, irradiated in long-term irradiation stations at JET during a JET D-D experimental campaign, have been condensed to a set of 11 distinct reaction rates with associated uncertainties. This data and the corresponding calculated response functions have been used together with a neutron spectrometry unfolding methodology, based on an iterative non-linear least squares algorithm, to derive, from an initial MCNP calculated ‘a priori’ neutron spectrum, an improved spectrum. These two spectra are compared and show that the largest fluence differences are in the energy region below 2 MeV, whereas in regions at and above 2 MeV better agreement is obtained, between 8–10%. It should be noted that the uncertainty in the KN1 fission yield counter calibration, which is used here to provide the measured neutron yield as input to the initial calculation, is approximately 10%. One can therefore conclude that, within the high energy regions at least, the calculations may be regarded as consistent with experiment. Efforts under the WPJET3 project to understand which geometric features and/or materials in JET MCNP models impact on the spectrum in the 0–2 MeV are ongoing in an attempt to obtain better agreement between calculation and experiment in



this energy region too.

Whilst the work presented here extends our previous work relating to the characterisation of JET irradiation stations, it also demonstrates that dosimetry foil activation measurements may be used as a complimentary integrated fluence measurement system for comparison with fission neutron yield counters, such as the KN1 system used in JET. Thus it is also highly relevant to ITER and DEMO neutron diagnostics of similar type. In addition to providing absolute measurements of neutron fluence the approach provides valuable neutron spectrum information, which has been extracted from the measurement data, particularly in energy regions above 2 MeV. The results may be used to interpret triton burn up levels for example. The spectrometry system and methodology detailed here is expected to be developed and refined further, through the upcoming JET D–D, T–T and D–T experiments and associated nuclear technology projects under WPJET3.

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