



EUROfusion

WPJET1-CPR(18) 18923

A Krivska et al.

RF Sheath Modeling of Experimentally Observed Plasma Surface Interactions with the JET ITER-Like Antenna

Preprint of Paper to be submitted for publication in Proceeding of
23rd International Conference on Plasma Surface Interactions in
Controlled Fusion Devices (PSI-23)



This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training programme 2014-2018 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.

This document is intended for publication in the open literature. It is made available on the clear understanding that it may not be further circulated and extracts or references may not be published prior to publication of the original when applicable, or without the consent of the Publications Officer, EUROfusion Programme Management Unit, Culham Science Centre, Abingdon, Oxon, OX14 3DB, UK or e-mail Publications.Officer@euro-fusion.org

Enquiries about Copyright and reproduction should be addressed to the Publications Officer, EUROfusion Programme Management Unit, Culham Science Centre, Abingdon, Oxon, OX14 3DB, UK or e-mail Publications.Officer@euro-fusion.org

The contents of this preprint and all other EUROfusion Preprints, Reports and Conference Papers are available to view online free at <http://www.euro-fusionscipub.org>. This site has full search facilities and e-mail alert options. In the JET specific papers the diagrams contained within the PDFs on this site are hyperlinked

RF Sheath Modeling of Experimentally Observed Plasma Surface Interactions with the JET ITER-Like Antenna

A. Krivská^{1,a)}, V. Bobkov², L. Colas³, P. Dumortier^{1,4}, F. Durodié¹, P. Jacquet⁴,
C. C. Klepper⁵, D. Milanesio⁶, G. Urbanczyk³ and JET contributors⁷

¹LPP-ERM/KMS, Royal Military Academy, 30 Avenue de la Renaissance B-1000, Brussels, Belgium

²Max-Planck-Institut für Plasmaphysik, D-85748 Garching, Germany

³IRFM CEA, Cadarache F-13108 Saint Paul lez Durance, France

⁴CCFE, Culham Science Centre, Abingdon, Oxfordshire OX14 3DB, UK

⁵Oak Ridge National Laboratory, Oak Ridge, Tennessee 37831-6169, USA

⁶Politecnico di Torino, Corso Duca degli Abruzzi 24, I-10129 Torino, Italy

⁷See the author list of “X. Litaudon et al 2017 Nucl. Fusion 57 102001

^{a)}Corresponding author: alena.krivska@rma.ac.be

Abstract. Waves in the Ion Cyclotron Range of Frequencies (ICRF) enhance local Plasma-Surface Interactions (PSI) near the wave launchers and magnetically-connected objects via Radio-Frequency (RF) sheath rectification. ITER will use 20MW of ICRF power over long pulses, questioning the long-term impact of RF-enhanced localized erosion on the lifetime of its Beryllium (Be) wall. Recent dedicated ICRF-heated L-mode discharges documented this process on JET for different types of ICRF antennas. Using visible spectroscopy in JET ICRF-heated L-mode discharges, poloidally-localized regions of enhanced (by ~ 2 -4x) Be I and Be II light emission were observed on two outboard limiters magnetically connected to the bottom of the active ITER-Like Antenna (ILA). The observed RF-PSI induced by the ILA was qualitatively comparable to that induced by the JET standard, type-A2 antennas, for similar strap toroidal phasing and connection geometries. The Be II line emission was found more intense when powering the bottom half of the ILA rather than its top half. Conversely, more pronounced SOL density modifications were observed with only top array operation, on field lines connected to the top half of the ILA. So far the near-field modeling of the ILA with antenna code TOPICA (Torino Polytechnic Ion Cyclotron Antenna), using curved antenna model, was partially able to reproduce qualitatively the observed phenomena. A quantitative discrepancy persisted between the observed Be source amplification and the calculated, corresponding increases in E_{\parallel} field at the magnetically connected locations to the ILA when changing from only top to only bottom half antenna operation. This paper revisits these current drive phased and half-ILA powered cases using this time flat model of the ILA and more realistic antenna feeding to calculate the E_{\parallel} field maps with TOPICA code. Further, the Self-consistent Sheaths and Waves for Ion Cyclotron Heating Slow Wave (SSWICH-SW) code, which couples slow wave evanescence with DC Scrape-Off Layer (SOL) biasing, is used to estimate the poloidal distribution of rectified RF-sheath Direct Current (DC) potential V_{DC} in the private SOL between the ILA poloidal limiters. The approach so far was limited to correlating the observed, enhanced emission regions at the remote limiters to the antenna near-electric fields, as calculated by TOPICA. The present approach includes also a model for the rectification of these near-fields in the private SOL of the ILA. With the improved approach we obtained good qualitative correlation between all experimental measurements and the calculated local variations in the E_{\parallel} field and V_{DC} potential.

1 Introduction

Waves in the Ion Cyclotron Range of Frequencies (ICRF) enhance local Plasma-Surface Interactions (PSI) near the wave launchers and magnetically-connected objects via Radio-Frequency (RF) sheath rectification. It is believed that the RF-PSI are mainly driven by parallel component of RF antenna electric near-field E_{\parallel} (parallel to confinement magnetic field of the tokamak). Progress in understanding pointed to the dominant role of induced currents in the antenna box as a main source of antenna E_{\parallel} fields [1]. E_{\parallel} field generates oscillations of voltages V_{RF} across a rectifying thin plasma boundary layers, called RF sheaths, where a line of the confinement magnetic field intercepts a conducting obstacle. Local sheath oscillations are subsequently rectified and lead to enhancement of the Direct Current (DC) plasma potentials V_{DC} . RF sheaths can develop over distances, ranging from a few centimeters up to several meters away from the ICRF antennas. The increased DC plasma potential accelerates ions that follow

the confinement magnetic field lines, hit the obstacle and cause enhanced erosion [2] and localized heat flux. Plasma ExB convection also results from DC electric fields $E_{DC} = -\text{grad}_{\perp}(V_{DC})$ arising from gradients in the DC potentials.

ITER will use 20MW of ICRF power over long pulses, raising concern over potential impact of RF-enhanced localized erosion on the lifetime of its actively-cooled Beryllium (Be) wall components. Recent, dedicated ICRF-heated L-mode discharges documented this process on JET for different types of ICRF antennas. Using visible spectroscopy, poloidally-localized regions of enhanced (by $\sim 2\text{-}4\times$) Be I and Be II light emission were observed on two outboard limiters magnetically connected to the bottom of the active ITER-Like Antenna (ILA) [3, 4]. Sequential toggling of the ICRF antennas combined with concurrent magnetic pitch-angle sweeping, consistently showed that these regions can be traced, via magnetic field-line connection, to regions of anticipated high E_{\parallel} RF near-field at an antenna mouth. The Be II line emission measured at K14 spot. It is horizontal, at outer wall directed at midplane, sightline #14 in charge-exchange recombination spectroscopy diagnostic. The Be II line emission was found more intense when powering the bottom half of the ILA rather than its top half. Conversely, more pronounced SOL density modifications were observed with lithium beam emission spectroscopy (Li-BES) system for only top array operation, on field lines connected to the top half of the ILA [5, 6]. Conversely, more pronounced SOL density modifications were observed with lithium beam emission spectroscopy (Li-BES) for only top array operation; its probing beam magnetically connects only to the top half of the ILA [7, 8].

The observed RF-PSI induced by the ILA were qualitatively comparable to those induced by the JET standard, type A2 antennas, for similar strap toroidal phasing and connection geometries [5, 6]. For the type A2 antennas, the observed, enhanced, long-range RF-PSI effect was shown to be consistent with E_{\parallel} near-field A2-specific antenna modeling with code TOPICA (Torino Polytechnic Ion Cyclotron Antenna) [9].

So far the near-field modeling of the ILA with TOPICA code, using curved antenna model, was partially able to reproduce qualitatively the enhancement of Be II light emission. A quantitative discrepancy persisted between the observed Be source amplification and the calculated, corresponding increases in E_{\parallel} field. The results showed increased E_{\parallel} fields at the area magnetically connected to K14 spot but there was no obvious difference in amplitude when changing from only top to only bottom half antenna operation. The experimental arrangement and results and indirect comparison with the calculated E_{\parallel} field maps are in detail described in [7]. This paper revisits these current drive-phased and half-ILA powered cases using this time flat model of the ILA with improved modeling inputs and more realistic antenna feeding for calculation of the E_{\parallel} field maps with TOPICA code. Further, the Self-consistent Sheaths and Waves for Ion Cyclotron Heating Slow Wave (SSWICH-SW) code [10] is used to estimate poloidal distribution of RF-sheath DC potential in the private SOL between the poloidal limiters of the ILA. The present approach includes also a model for the rectification of these near-fields in the private SOL of the ILA. First simulations of the ILA curved model with SSWICH-SW code for various full antenna feeding were presented in [11]. With the improved approach we obtain good qualitative correlation between all experimental measurements and the calculated local variations in the E_{\parallel} field and V_{DC} potential. This work helps to study the formation of RF sheaths around the antenna and magnetically connected objects.

2 Description of the simulations

The ILA was reinstalled for the 2015 JET experimental campaign [12] with ITER-like wall. It uses compact phased arrays of poloidal current straps to launch Fast Wave. Evanescent Slow Wave is excited parasitically. The ILA has successfully been operated with power densities up to 6.2 MW/m^2 on L-mode and 4.1 MW/m^2 on H-mode and voltages up to 42 kV [13]. Detailed description of the antenna system can be found in [14].

Calculation of E_{\parallel} field maps at the ILA mouth was performed with TOPICA code using improved modeling inputs and more realistic antenna feeding. In TOPICA code, the problem is separated into two parts. The antenna, which is assumed to be in vacuum, is treated in spatial domain, while the spectral domain is adopted to evaluate the interaction with plasma inside the toroidal chamber. Field continuity and boundary conditions allow formulating of a set of two coupled integral equations for the unknown equivalent current sources; then the equations are reduced to a linear system by a method of moments solution scheme employing 2D finite elements defined over a 3D non-planar surface triangular-cell mesh. Accurate plasma modelling was obtained by coupling the plasma description of the FELICE code [15] to TOPICA. If the plasma boundary surface is curved a convenient geometrical ‘stretching’ is applied on it and the plasma is considered plane and transversely unbounded. Detailed code description can be found in [9].

To avoid possible errors related to dealing with a curved geometry, this time we used flat model of the ILA (Fig. 1a) with flat plasma boundary surface. It includes radially protruding limiters and side walls, which represent two Faraday screens of the adjacent A2 antennas. The vacuum-plasma interface was placed 1 cm in front of the leading

edge of the long poloidal limiters. First surface where we compute the E_{\parallel} field was defined in the vacuum region 5 mm behind the vacuum-plasma interface. Second surface for the E_{\parallel} field calculations was placed between the poloidal limiters, 5 mm behind their leading edge and 3 mm above the leading edge of the antenna frame as sketched in Fig. 1b. E_{\parallel} maps evaluated on the second surface were used as the main input to estimate distribution of the RF-sheath potential V_{DC} in the private SOL between the poloidal limiters of the ILA. For this purpose we used the asymptotic version of the SSWICH-SW code with radiating boundary conditions, which couples slow wave evanescence with Direct Current (DC) Scrape-Off Layer (SOL) biasing. Only Slow waves, from a given TOPICA E_{\parallel} field map, propagate to plasma-facing boundaries in the launcher vicinity, cause sheath RF oscillations there. The code only includes a model for the rectification of these near-fields in the private SOL of the ILA, while measurements were performed in the free SOL. But from earlier simulations on Tore Supra [16] and ASDEX Upgrade [17] we expect similar poloidal structures of the DC potentials in the free and private SOL, despite smaller absolute values. Sketch of the simulation domain can be found in [6]. The SSWICH-SW code was chosen because it is suitable for relative comparisons of antenna designs and electrical settings. Main disadvantages are number of approximations made on the original physical model. Parallel DC plasma conductivity is taken as infinite while transverse plasma conductivity is neglected in the simplified model of DC plasma biasing.

New plasma kinetic profiles for L-mode JET pulse #90454 with varying safety factor at 95% of the flux surface q_{95} from 3.04 to 3.92 were generated separately for top and bottom coordinates of the ILA. Plasma density profiles were measured with reflectometer and plasma temperature profiles were obtained with ECE Michelson interferometers. For all the kinetic profiles the antenna-plasma radial outer gap distance was equal to 6 cm, central plasma density was around $3.35 \cdot 10^{19} \text{ m}^{-3}$ and central plasma temperature was 1.6 keV. Central static magnetic field was 2.5 T, 10° tilted with respect to the toroidal direction. In the simulations plasma geometry was assumed slab with temperature and density gradients along minor radius of the tokamak chamber. Simulations were performed for working frequency 42 MHz and minority heating scheme with 3.5% of hydrogen and 96.5 % of deuterium.

The ILA is a complex 3D geometry object installed in the machine. The exact antenna dimensions and position were not known because of the manufacturing and mounting tolerances. For the antenna modeling, it is necessary to know the position of the plasma kinetic profiles w.r.t the antenna front face. Before running the new simulations, an in-vessel survey was carried out and the exact actual position of top, middle and bottom part of the antenna in the machine was determined.

To determine the realistic antenna feeding voltages for given antenna scattering matrix and operational parameters, a fully comprehensive circuit and simulation model for the ILA [18] has been implemented. The antenna scattering matrix was obtained from numerical simulations by TOPICA taking into account the experimental kinetic profile in front of the antenna. This scattering matrix together with measured operational parameters such as the frequency, the power, the T-junction impedance and the phasing of the antenna are the input of the ILA circuit simulation programme used to evaluate the realistic antenna feeding. The realistic antenna feeding voltages for current drive strap phasing ($0 - \pi/2$), corresponding to measured coupled power to plasma, was applied for only top and only bottom half array of the antenna. The complete description of the simulation process is summarized in the flow diagram shown in Fig. 3.

3 Simulation results

3.1 Distribution of E_{\parallel} near field

Distributions of absolute value of E_{\parallel} near field calculated 5 mm in front of the leading edge of the poloidal limiters of the ILA with TOPICA code are presented in Fig. 4. These results were obtained for kinetic profiles with $q_{95} = 3.32$. The red dots show the area that is magnetically connected to K14 spot where the local Be II line emission was spectroscopically measured. Fig. 4a) shows E_{\parallel} field map for ($0 - \pi/2$) phasing, only top antenna feeding and coupled power to plasma $P = 550 \text{ kW}$. Increased E_{\parallel} fields are located along the poloidal limiters and the highest values are in the top part. Fig. 4b) shows E_{\parallel} field map for ($0 - \pi/2$) phasing, only bottom antenna feeding and coupled power to plasma $P = 490 \text{ kW}$. Increased E_{\parallel} fields are located along the poloidal limiters too but the peak values are in the bottom part. The field imbalance between the left and right side visible in Fig. 4b) is due to larger imbalance in strap feeding voltages. In current drive operation there is 90° difference between the left and the right antenna straps and mutual coupling is high. Due to it the antenna system tends to be more sensitive to small differences in phasing and feeding voltages can be less balanced. During the experiment the feeding voltages were less balanced when operating only lower antenna half. The higher fields are assumed to be mainly due to image current

densities circulating on the passive antenna limiters. At the area magnetically connected to K14 spot the maximum $E_{||}$ field is about 2x higher for only bottom than for only top feeding.

3.2 Distribution of RF-sheath DC potential

Radial-poloidal distribution of RF-sheath DC potential V_{DC} in the private SOL between the ILA poloidal limiters for $(0 -\pi/2)$ phasing and only top and only bottom half array antenna feeding are depicted in Fig. 5. Potential V_{DC} appears over the whole poloidal height of the side limiters, and not only in front of the radiating straps. Presented results were obtained for kinetic profiles with $q_{95} = 3.32$. Tab. 1. shows maximum V_{DC} at area magnetically connected to K14 spot for all considered kinetic profiles and feeding. In all cases the potentials exceed the threshold for sputtering Be with D^+ ions. The maximum V_{DC} potentials are by ~ 1.6 - 2.2 x higher for only bottom than only top antenna feeding. Fig. 6. presents 1D RF-sheath DC potential, averaged in radial direction, for $(0 -\pi/2)$ phasing and both half array antenna feedings. The peak values of V_{DC} potentials are in poloidal direction from $y = 0.7$ m to $y = 1.2$ m for only top and from $y = -0.7$ m to $y = -1.2$ m for only bottom array feeding.

Profile and feeding	Max V_{DC} [V]
$q_{95} = 3.92$, only top	220
$q_{95} = 3.42$, only top	300
$q_{95} = 3.32$, only top	340
$q_{95} = 3.92$, only bottom	350
$q_{95} = 3.42$, only bottom	600
$q_{95} = 3.32$, only bottom	735

Tab. 1. Maximum V_{DC} at area magnetically connected to K14 spot

4 Conclusion and discussion

Distributions of $E_{||}$ near field and V_{DC} potential in the private SOL between the ILA poloidal limiters were calculated for $(0 -\pi/2)$ phasing and half antenna feeding using the ILA flat model and improved realistic modeling inputs. Areas with increased values of $E_{||}$ fields and V_{DC} potential were identified. For only top/only bottom feeding, the peak $E_{||}$ and V_{DC} values are not localized in front of the active straps but they are localized in the top/bottom part of the ILA poloidal limiters, respectively. Higher V_{DC} potential values were obtained for the kinetic profiles with lower q_{95} . The maximum V_{DC} potentials at area magnetically connected to K14 spot are by ~ 1.6 - 2.2 x higher for only bottom than only top antenna feeding. The Be II line emission measured at K14 spot (understood as local, RF sheath-enhanced erosion) was found by ~ 2 - 4 x more intense when powering the bottom half of the ILA rather than its top half. Further, more pronounced SOL density modifications were observed with Li-BES system for only top array operation, on field lines connected to the top half of the ILA. With the updated approach we obtained good qualitative correlation between all experimental measurements and the calculated local variations in the $E_{||}$ field and V_{DC} potential.

Using the flat model geometry leads to results which are in better agreement with experiments than using the curved geometry even when we apply almost the same mesh density on the antenna model and the same plasma input parameters. The reasons are not fully clear and further investigations are ongoing. First possible reason could be related to mesh density which could become insufficient when the antenna geometry and the vacuum-plasma boundary surface are curved. This could lead to errors in simulation and part of other electric field component could be included to $E_{||}$ component during post-processing. This hypothesis could be tested by creating and simulating more simple and smaller curved and flat antenna models. Mesh density on the vacuum-plasma interface could be increased and influence on the results would be observed. So far in our simulations of the detailed ILA model, we applied the highest possible mesh density on the vacuum-plasma interface. This density is limited by the memory of the computing node on the supercomputer cluster.

Second possible explanation could be related to the stretching procedure implemented to couple 3D TOPICA with the 1D FELICE plasma model, which may lead to an approximation error above all on the poloidal component, i.e. where the antenna curvature is stronger. Unfortunately, the only way to verify this is to couple a 3D plasma

model (or even 2D with only poloidal density variation), which is currently not supported by TOPICA code. To overcome this limitation, the E_{\parallel} field of the ILA could be computed using other simulation tool such as RAPLICASOL (Radiofrequency wAve couPLing for Ion Cyclotron Antenna in Scrape-Off-Layer) [19]. It is a finite element solver for Maxwell's equations in the cold plasma approximation. It was recently extended to be able to handle 3D plasma density profiles [20].

All the presented calculations of V_{DC} potentials were performed with asymptotic version of the SSWICH-SW code. Absolute values of V_{DC} potentials are probably over-estimated with the present calculations, that do not allow for transverse transport of DC currents. Further, the radial extent of the density perturbation in front of the antenna limiters cannot be presently reproduced. In the next step we will use for simulations a more complete version of SSWICH-SW code [19] which includes finite DC transverse conductivity and allows to calculate the V_{DC} potentials not only between the antenna limiters but also in free SOL around the limiters and antenna central septum. We also plan to investigate how distributions of E_{\parallel} field and V_{DC} potential change with varying frequency, wall clearance and plasma parameters.

Acknowledgment

This work has been carried out within the framework of the EUROfusion Consortium and has received funding from the Euratom research and training programme 2014-2018 under grant agreement No 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission.” This work has been carried out using Cineca's supercomputer system Marconi.

References

- [1] L. Colas et al., Nucl. Fus. 45, 767 (2005)
- [2] C.C. Klepper, D. Borodin et al., Phys. Scr. T167 (2016) 014035
- [3] C.C. Klepper et al., J. Nucl. Mater. 438, S594–S598 (2013)
- [4] C.C. Klepper et al., Phys. Scripta, vol. 2016, no. T167 (2016) 014035
- [5] C.C. Klepper et al., EPJ Web of Conferences 157, 03024 (2017)
- [6] P. Jacquet et al., EPJ Web of Conferences 157, 02004 (2017)
- [7] L. Colas et al., to be presented at “2D mappings of ICRF-induced SOL density modifications on JET” proc. 45th EPS conference on Plasma Physics, Prague 2018, O4.101, <http://ocs.ciemat.es/EPS2018PAP/pdf/O4.101.pdf>
- [8] V. Bobkov et al., submitted to Nuclear Materials & Energy
- [9] V. Lancellotti, D. Milanesio, R. Maggiora et al., Nucl. Fus. 46, S476 (2006)
- [10] L. Colas, J. Jacquot, S. Heuraux et al., Phys. Plasmas 19 092505, (2012)
- [11] A. Křivská et al., EPJ Web of Conferences 157, 03026 (2017)
- [12] P. Dumortier et al., Fusion Eng. Des. 123, 285-288 (2017)
- [13] F. Durodié et al., Plasma Phys. Control. Fusion 54, 7 (2012)
- [14] F. Durodié et al., Fusion Eng. Des. 74, 223–228 (2005)
- [15] M. Brambilla, tech. rep., IPP, 1992.
- [16] J. Jacquot et al. Phys. Plasmas 21, 061509 (2014)
- [17] A. Křivská et al., AIP Conference Proceedings 1689, 050002 (2015)
- [18] F. Durodié et al., Proc. 20th Top. Conf on RF power in Plasmas, AIP Conf. Proc. 1689, 070013 (2015)
- [19] J. Jacquot et al., AIP Conference Proceedings, Vol. 1689, p. 050008 (2015)
- [20] W. Tierens et al., EPJ Web of Conferences 157, 03053 (2017)

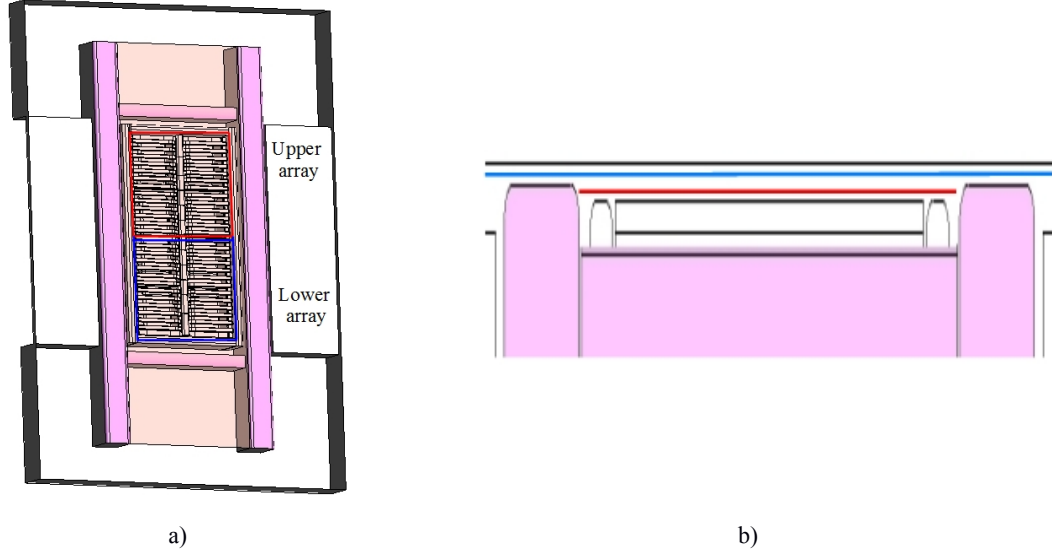


Fig. 1. a) Flat model of the ILA, b) side view (zoomed and elongated) with limiters and antenna frame, vacuum-plasma boundary is in black, first surface for $E_{||}$ calculations above the limiters is in blue, surface for $E_{||}$ calculations between the limiters is in red (corresponding to $x=0$ on figure 5).

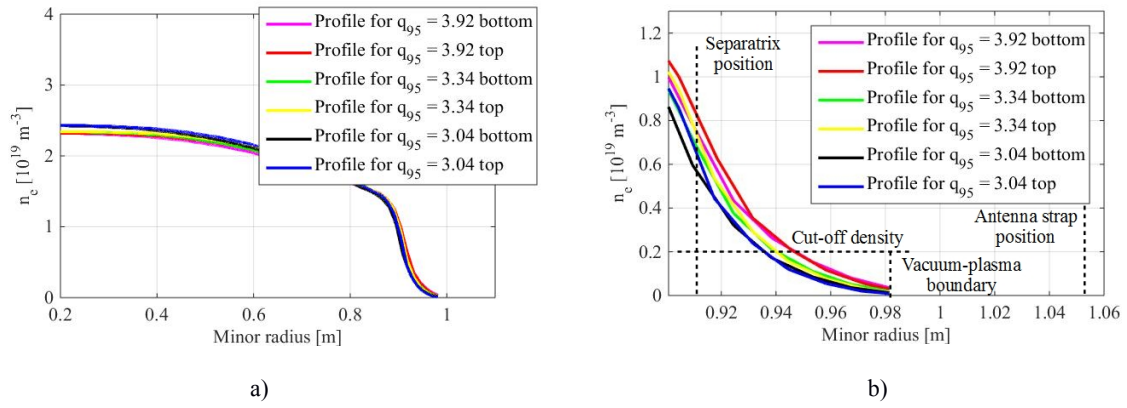


Fig. 2. a) Electron density profiles with varying q_{95} that were measured during shot #90454 with reflectometer KG10 separately for top and bottom coordinates of the ILA. b) Detail of the edge density profiles.

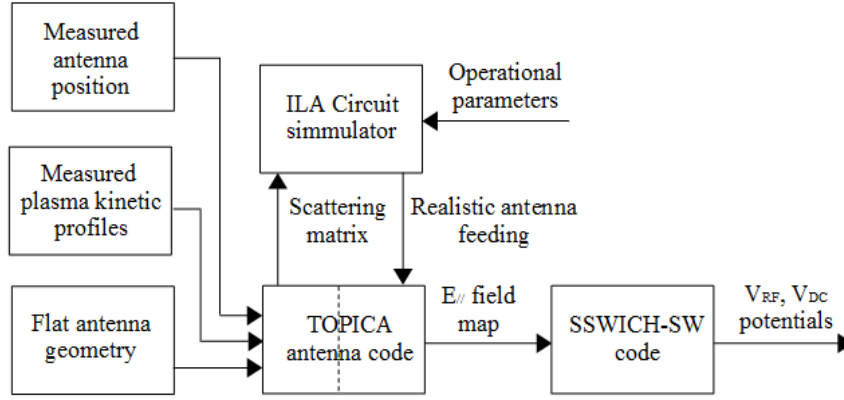


Fig. 3. Flow diagram of the complete description of the simulation process.

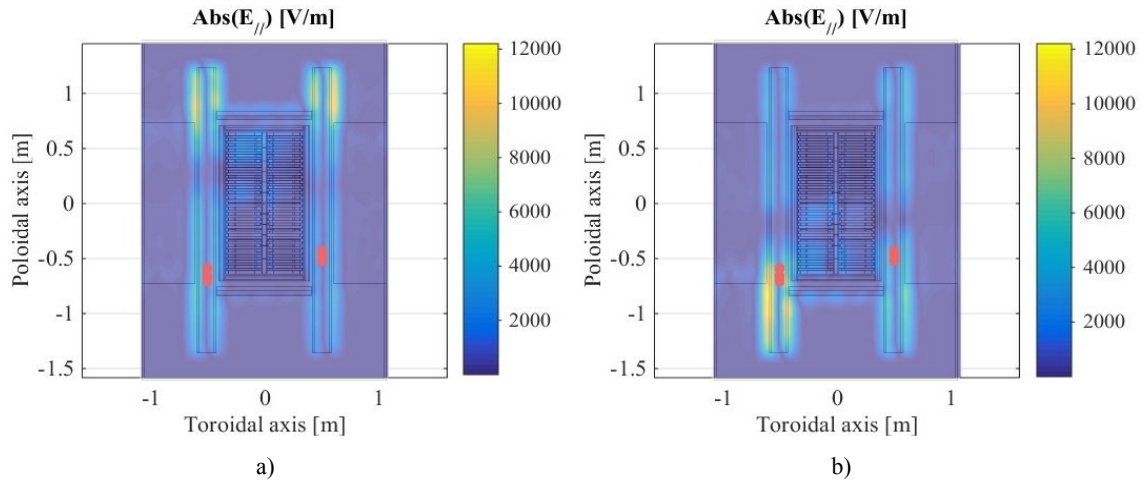


Fig. 4. Distribution of absolute values of $E_{//}$ field for $(0 -\pi/2)$ phasing and a) only top and b) only bottom half array antenna feeding. The results were obtained for density profiles with $q_{95} = 3.32$. Red lines: zone on antenna limiters connected magnetically to visible spectrometer spot K14.

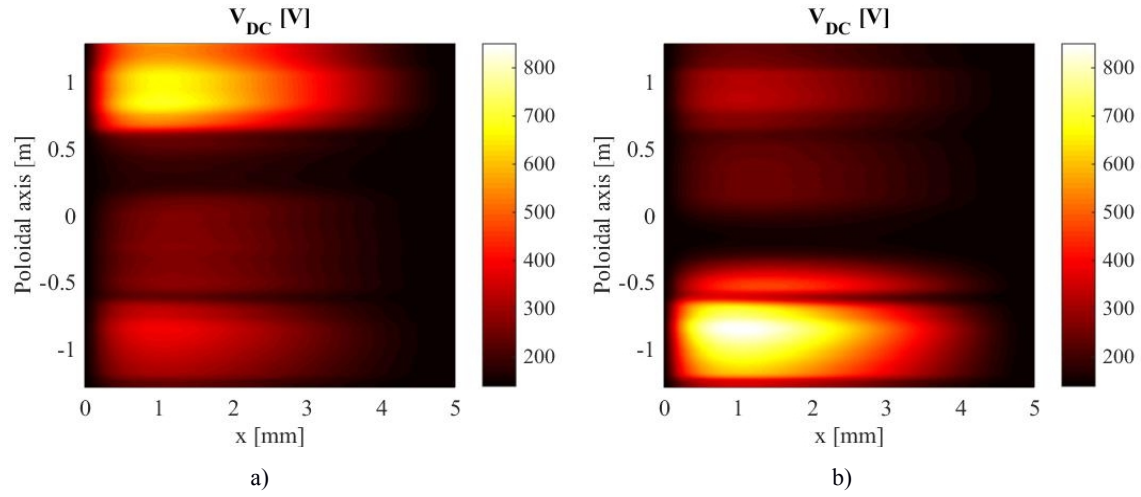


Fig. 5. Radial-poloidal distribution of RF-sheath DC potential for $(0 - \pi/2)$ phasing and a) only top and b) only bottom half array antenna feeding. The results were obtained for density profiles with $q_{95} = 3.32$. $x = 0$ mm in the radial direction corresponds to location 5 mm behind the leading edge of the poloidal limiters (red line on figure 1), $x = 5$ mm corresponds to the leading edge of the poloidal limiters.

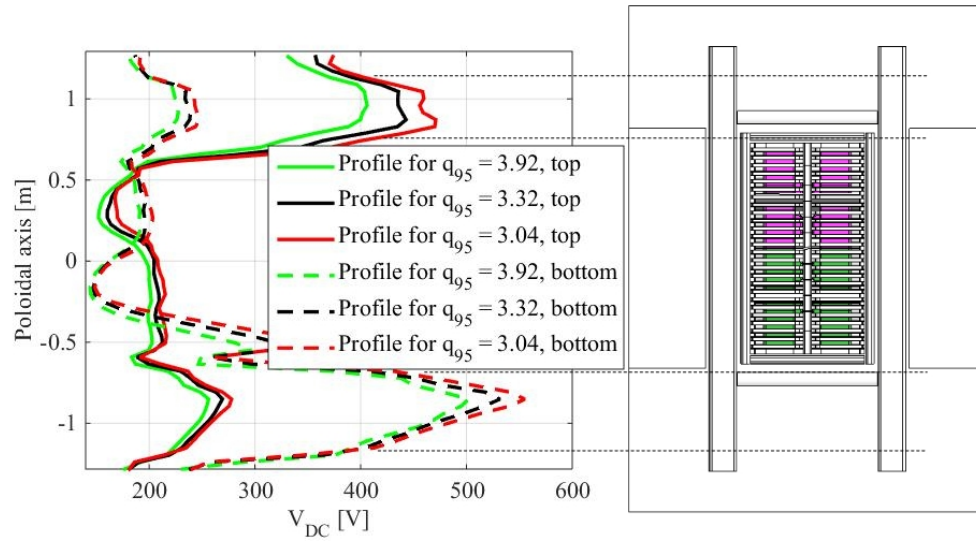


Fig. 6. 1D RF-sheath DC potential, averaged in radial direction, for $(0 - \pi/2)$ phasing and both half array antenna feedings.