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\*See appendix of the paper by J.Pamela "Overview of recent JET results",  
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## 1. INTRODUCTION.

For the extrapolation to future large fusion devices, similar scenarios on different size tokamaks are essential to investigate the formation process, power threshold and steady state prospects of Internal Transport Barrier (ITB). In the 2000 JET campaigns, dedicated experiments have attempted to reproduce the ASDEX-Upgrade stationary advanced scenario [1].

In addition to extending the domain of existence of ITBs in JET to the  $q = 1$  integer surface, the experimental similarities between ASDEX Upgrade and JET suggest that these advanced regimes may have the same underlying physics.

## 2. JET Q=1 ITB SCENARIO.

Experiments performed in ASDEX-upgrade ( $a = 0.5$ ;  $R = 1.65$ ) have achieved stationary regime with high performance ( $H_{\text{ITER89-P}} = 3.0$ ;  $\beta_N = 2.4$ ;  $T_i(0) = 10\text{keV}$ ;  $T_e(0) = 5\text{keV}$ ) and  $q(0)$  in the vicinity of 1 [1]. This regime is accompanied by  $n = 1$ ,  $m = 1$  fishbone activity and core confinement transition, which at constant heating power becomes noticeable as a peaking of electron and ion temperature and density profiles, and is correlated with an increase of the neutron rate. In JET ( $a = 0.95$ ;  $R = 2.96$ ), this regime has been reproduced and shows similar features than those observed in ASDEX-Upgrade (Fig 1). As  $q_0$  reaches 1,  $n = 1$ ,  $m = 1$  fishbone activity is also triggered. In this phase the  $q$  profile evolution is consistent with the presence of a reconnection-like process. Simulations of the current diffusion with the JETTO code without reconnection mechanism show a continuous drop of central  $q$  value. Reconnection is therefore necessary to explain that  $q_0$  stays close to for more than 1 second, like the ASDEX-Upgrade scenario [1]. In comparison to the ASDEX-Upgrade scenario, the performance of the JET regime are rather modest ( $H_{\text{ITER89-P}} = 2.0$  and  $\beta_N = 1.4$ ). However, in JET a clear ITB is formed in the main heating phase at 7.4s prior to the first fishbone. During the ITB phase  $T_i(0)$  reaches 15keV and  $T_e(0)$  10keV for an average density ( $n_e = 2.5 \cdot 10^{19} \text{ m}^{-3}$ ) lower than in the ASDEX-Upgrade scenario ( $n_e = 4 \cdot 10^{19} \text{ m}^{-3}$ ). The ITB triggering appears to be correlated with the presence of the  $q = 1$  surface ( $r/a = 0.35$ ) as observed on ECE and soft X-ray measurements. This new experiment is a further indication that the role of integer  $q$  surfaces in the ITB triggering unveiled in previous works [2,3] is not limited to the  $q = 2$  or  $q = 3$  surfaces. This suggests that the role of integer  $q$  surfaces in the ITB triggering physics in JET is quite general.

## 3. TRANSPORT ANALYSIS AND ITB IDENTIFICATION.

To confirm the presence of a core transport barrier, a TRANSP analysis has been carried out for Pulse No: 51860 using the equilibrium data from the EFIT code combined with Motional Stark Effect diagnostic (MSE). The ion temperature data were provided by the charge-exchange recombination spectrometer and electron temperature data from Thomson scattering. As illustrated in Fig. 2, the ion diffusion coefficient is strongly reduced when the barrier forms and gets close to its neo-classical value in the plasma core.

The presence of the ITB in JET is also confirmed by the ITB quantitative criterion characterised by the parameter  $\rho_T^* = \rho_s / L_T$  [4] (Fig. 3). This criterion compares the typical drift wave (such as ion temperature gradient instability: ITG [6]) scale length  $\rho_s$  with the local temperature gradient length  $L_T$ . When this quantity exceeds a threshold value of 0.014 in JET, the analysis shows that ITB are formed as the result of the possible stabilisation of ITG by  $E \times B$  rotational flow and magnetic shear effects.

In ASDEX-Upgrade, the temperature profiles of improved confinement H-mode are observed to be stiff [5] (i.e. one can scale the profiles at any time with a single multiplication factor). The profile stiffness is in qualitative agreement with the ion temperature gradient instability (ITG) models. For flat (or almost flat) density profiles the criterion for the ITG instability is reduced to a critical ion temperature gradient length expressed as  $R/L_{Ti}$ . When this critical gradient is exceeded the profile clamps to the critical gradient length. This feature has been used to identify the presence of ITB in the reversed shear scenario in ASDEX-Upgrade [6]. Indeed, in presence of strong  $E \times B$  shearing rate the ITG turbulence could be stabilised and the ion temperature profile stiffness can be broken.

In the case of the ASDEX Upgrade  $q = 1$  improved confinement H-mode, the ion temperature has not been found to deviate significantly from the profile stiffness on the  $T_i(0)$  versus  $T_i(r/a = 0.8)$  diagram. The same analysis has been made for JET using a large database of ELMy and Hot-Ion H-modes (Fig. 3). The data are showing a stiffness “trend” except at high temperature. The critical value of  $R/L_{Ti} = 5.5$  for JET is consistent with both the expected linear kinetic threshold for ITG [6] and the value of ASDEX-Upgrade ( $R/L_{Ti} = 6.5$ ) given its larger aspect ratio (3.3 for AUG and 2.9 for JET). On the diagram of Fig. 4, the time trajectories of two JET ITBs are also super-imposed. Pulse No: 51573 is a typical reversed shear ITB case with Lower Hybrid preheat [8] ( $B_T = 2.6T; I_p = 2.3MA; P_{IH} = 15MW$ ) associated with the  $q = 2$  surface. It is clearly drifting away from the observed profile stiffness trend. The JET  $q = 1$  ITB scenario (see Fig. 1) is also showing a bifurcation behaviour from the stiffness trend which confirms again that an ITB is formed for this type of scenario. Using this type of comparative analysis, the physics understanding of ITB formation could benefit greatly of common experiments performed on two different size devices.

#### 4. JET – ASDEX-UPGRADE DIFFERENCES FOR ITB SIMILAR EXPERIMENTS.

From the TRANSP analysis, the non-inductive current contributions to the total current in JET are also compared with the equivalent analysis done by ASTRA in ASDEX-Upgrade in Fig. 5a and 5b. Although the  $q$  profile on both devices are close to 1 in the plasma core and at the edge ( $q_{95} = 4.0$  for ASDEX-Upgrade and 3.2 for JET), the ASDEX-Upgrade current density profile is clearly more peaked than the JET profile. This is also supported by the difference of internal inductance (0.9 for JET and 1.1 for AUG). This difference is most likely due to the difference in resistive skin time on the two machines due to their different plasma radius (0.95 for JET and 0.5 for AUG). Since the current profile is recognised as one of the most important plasma parameters to produce ITBs, to get

closer to actual ITB identity experiments on both machines, it is necessary to match the target  $q$  profiles ( $q_0$ ,  $q_{\min}$  and  $q_{95}$ ) and the plasma configuration. This task is complicated by the different resistive skin times and operational constraints. The  $q$  profile build-up depends strongly on the available heating schemes as well. Electron Cyclotron heating in ASDEX-Upgrade or Lower Hybrid in JET can play a key role in pre-forming the target  $q$  profile [8]. The neutral beams are also playing a key role in ITB production through the applied torque and particle fuelling. Their technical characteristics (orientation, power and energy) are therefore essential to achieve the similar  $E \times B$  shearing rate and fuelling rate on both devices. Identity experiments matching the normalised Larmor radius  $\rho^*$  appear also possible provided that JET operates at low toroidal field (typically 1.7T) and ASDEX-Upgrade at 3.0T. However, this implies for JET a higher sensitivity to the ELM activity [9] which could affect the ITB existence.

## CONCLUSIONS

JET and AUG common  $q = 1$  advanced scenario on JET and AUG are showing similar features (current profile behaviour around  $q = 1$ , fishbone activity etc). In JET, a  $q = 1$  ITB has been produced and shows the same features as ITBs related to other integer  $q$  like  $q = 2$  and  $q = 3$  achieved in JET. On the basis of this  $q = 1$  scenario, and given their characteristics, JET and AUG do have the potential to study a large spectrum of identical current density profiles and configurations for overlapping range of  $\rho^*$  to perform real identity experiments.

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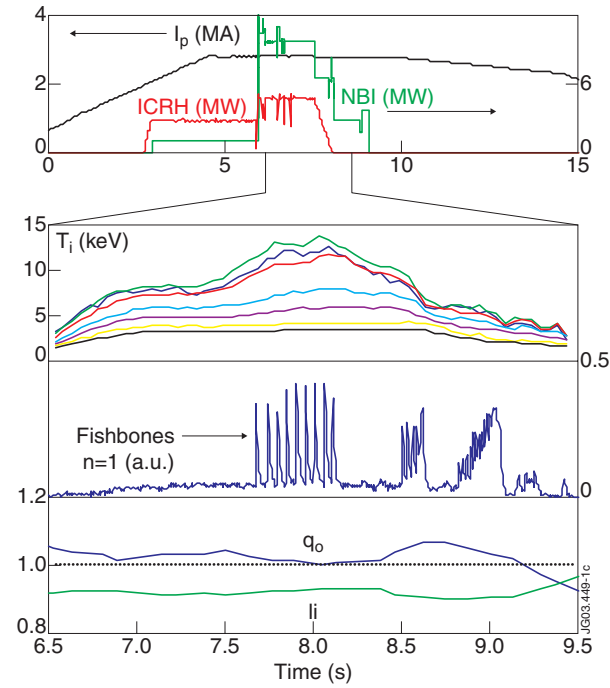


Figure 1: Typical  $q = 1$  ITB scenario in JET.

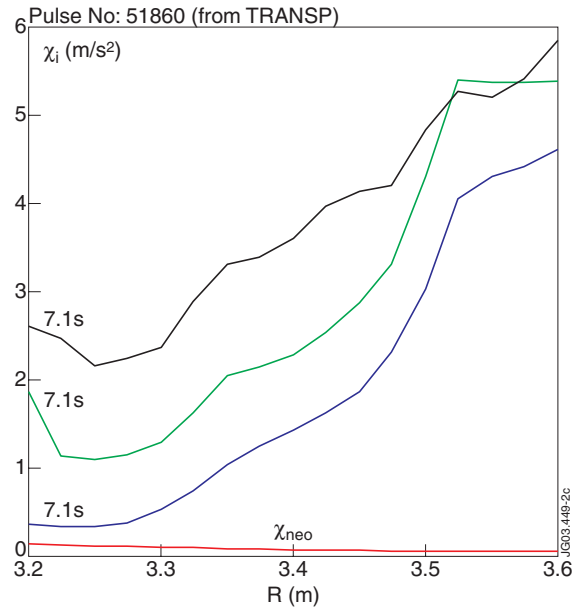


Figure 2: Evolution of the ion diffusivity profiles from TRANSP.

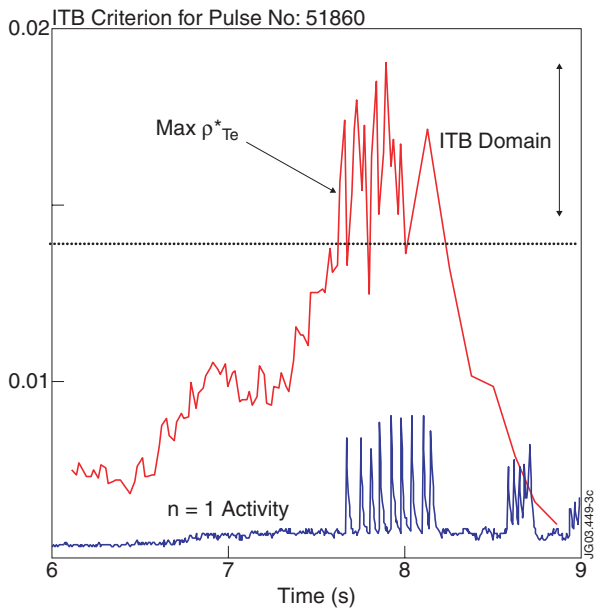


Figure 3: Time evolution of the maximum value of ITB criterion for electrons  $\rho^*_{Te} = \rho_{se} / L_{Te}$ . The fishbone  $n = 1$  activity is also shown.

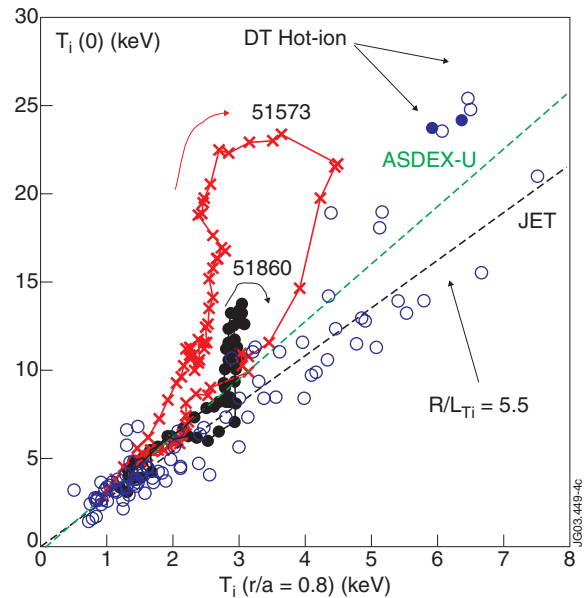


Figure 4:  $T_i(0)$  versus  $T_i(r/a = 0.8)$  diagram for JET using ELMy and Hot-Ion H-mode data. A profile stiffness “trend” is observed on JET except at high temperature and for DT pulses.  $q = 1$  ITBs (Pulse No: 51860) and  $q = 2$  ITBs (Pulse No: 51573) are breaking the profile stiffness.



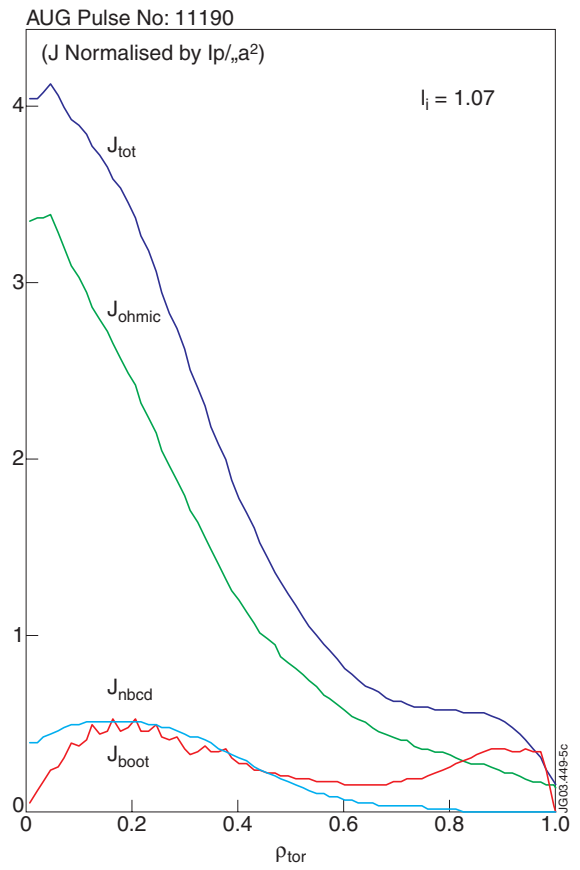
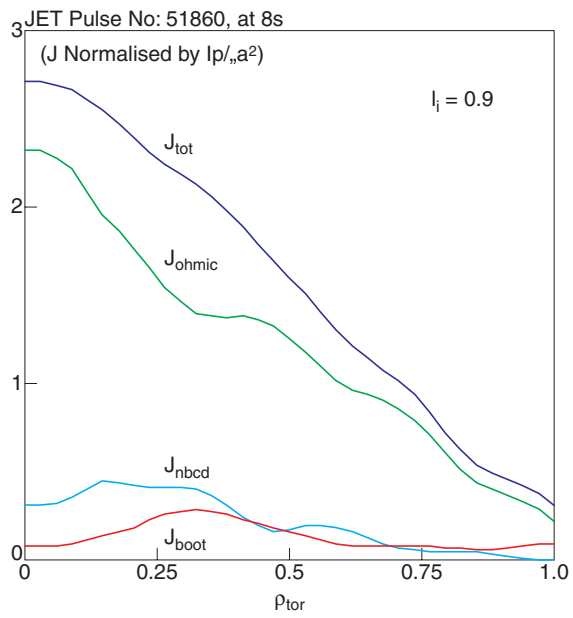


Figure 5a and 5b: Comparison of the current diffusion analysis from TRANSP (for JET;  $P_{NBI} = 10\text{MW}$ ) and ASTRA (for ASDEX-Upgrade  $P_{NBI} = 5\text{MW}$ ) for the  $q = 1$  scenario.